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# Fibre-based packaging and barrier coatings: influence on the converting and recycling

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# AGENDA

- Context
- Materials
- **Converting: heat-sealing, folding, creasing, tray forming**
- **Recyclability: UNI 11743 and Aticelca 501, CEPI v.2 and 4evergreen**
- Conclusions





### **Fibre-based packaging**

Paperisation process, where polymeric packaging is substituted with fibre-based counterparts

### **Monomaterial:**

non-cellulosic content < 5%

### **Recyclable:**

Different testing methodologies, e.g., CEPI version 2 and UNI 11743

- **Reduced non-cellulosic content**
- **Thinner coatings**
- **Inorganic/Mineral coatings**
- **Nanomaterials\***

\* There still exist issues for applications in food packaging

## CONTEXT

### One possible solution

Dispersion coatings are waterborne dispersions composed of a polymeric latex, possible filler, and other chemicals

#### Advantages:

- Applied on the substrate using conventional printing technologies
- Low dry coat grammages

#### Disadvantages:

- Typically, more expensive as against extruded or laminated coatings
- Coating evenness influenced by substrate/primer

Dispersion coatings can provide good barrier properties, but

**how do they behave  
when converted  
or recycled?**

# MATERIALS

**Substrates:** Paper (125 g/m<sup>2</sup>) and paperboard (350 g/m<sup>2</sup>) substrates

**Dispersion coatings:** commercial (SA-B1, A-H, SA-H, SAP-H), and experimental grades filled with kaolin

Single layer application with **rod coating** technology at a laboratory scale

Conditioning and testing at 23±1 °C and 50±2% relative humidity.

	Grammage [g/m <sup>2</sup> ]	Thickness [μm]	Bendtsen roughness [mL/min]	Bendtsen air permeability [μm/(Pa·s)]
<b>KBa</b>	125.1 ± 1.83	146 ± 1	217.1 ± 20.7	1.634 ± 0.119
<b>TF</b>	348.4 ± 2.9	458 ± 3	390 ± 72	4.317 ± 0.175
<b>TF PET</b>	386.9 ± 2.7	488 ± 4	349 ± 106 *	0.244 ± 0.012 *

\* The values were obtained by measuring the PET-coated side.

	Polymer	Pigment	Solid content [%]	T <sub>g</sub> [°C]
<b>SA-B1</b>	Styrene acrylate	None	46.1	31.7
<b>A-H</b>	Acrylate	None	38.8	47.1 / 75.2
<b>SA-H</b>	Styrene acrylate	None	49.6	-6.1 / 39.1
<b>SAP-H</b>	Styrene acrylate	Alumino-silicate	50.9	12.1
<b>H39K 100</b>	Styrene butadiene	None	53.6	-0.6 / 19.0
<b>H39K 80</b>	Styrene butadiene	Kaolin (20 w%)	50.0	-0.6 / 19.0
<b>H39K 60</b>	Styrene butadiene	Kaolin (40 w%)	50.0	-0.6 / 19.0
<b>H39K 40</b>	Styrene butadiene	Kaolin (60 w%)	50.0	-0.6 / 19.0



# **CONVERTING PROPERTIES**

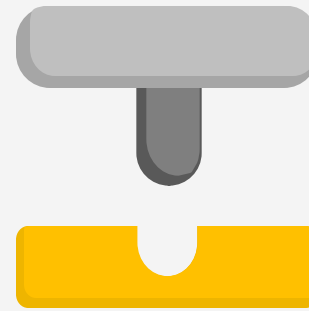
# CONVERTING PROPERTIES AND TRAY FORMING



**Heat-sealing**



**Fold cracking**



**Creasing**



**Tray forming**

# CONVERTING PROPERTIES AND TRAY FORMING



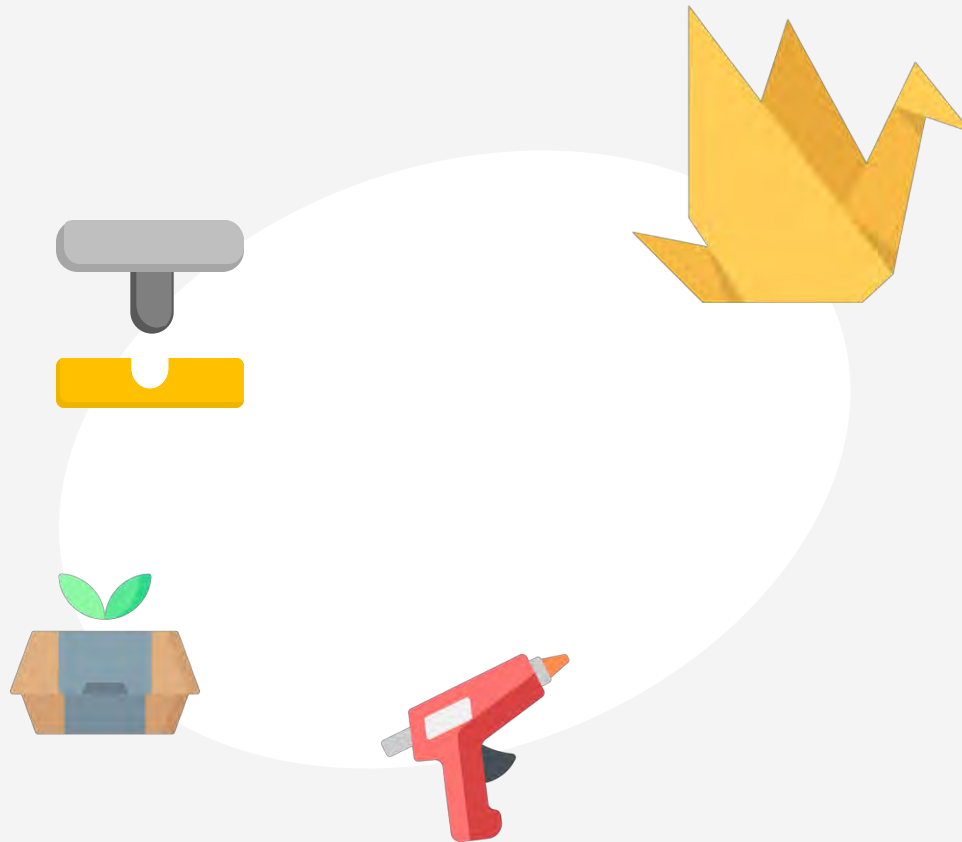
## Heat-sealing

Involves the softening and sealing of a thermoplastic polymer. Process parameters include **sealing temperature, time, and pressure**

Top tool: heated, flat. Bottom tool: flexible.  
Measured with an **unsupported T-peel test**



# CONVERTING PROPERTIES AND TRAY FORMING



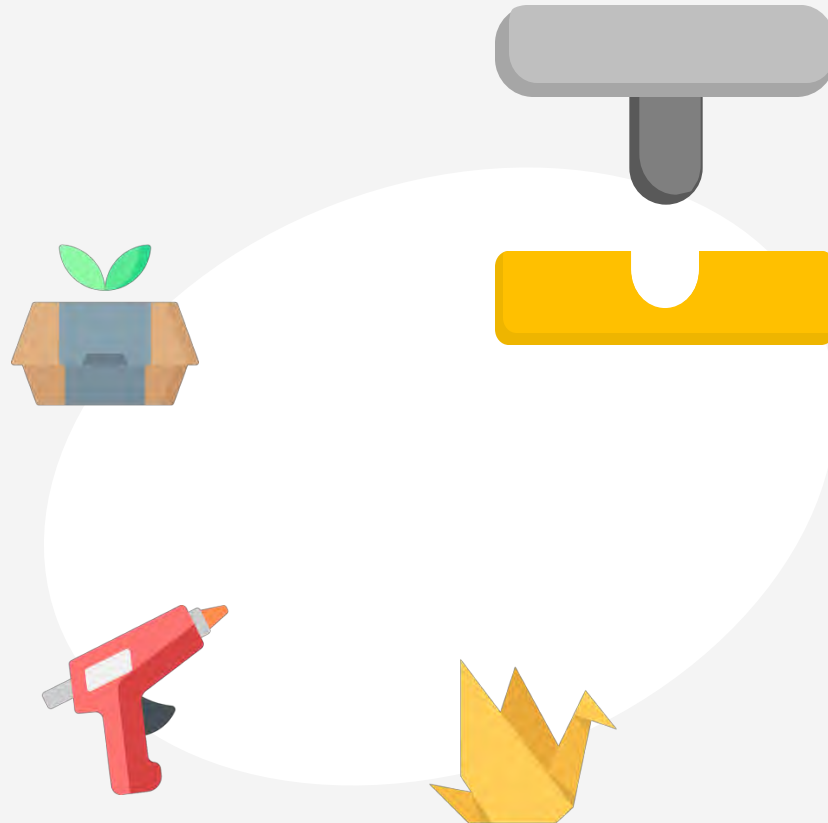
## Folding

Involves tensile (compression) stresses on the outside (inside) of the fold line. It is influenced by the **coating orientation** and the **fold line orientation**, in addition to material properties and pressing speed and force.

Typically, fold cracking resistance testing is not standardised. In this study: a force of 10 N is applied along the fold line for 1 s; fold cracking assessed through optical measurement.

# CONVERTING PROPERTIES AND TRAY FORMING

In collaboration with:



## Creasing

Performed to locally reduce bending stiffness of, e.g., paperboard and board through **delamination of the substrate layers**.

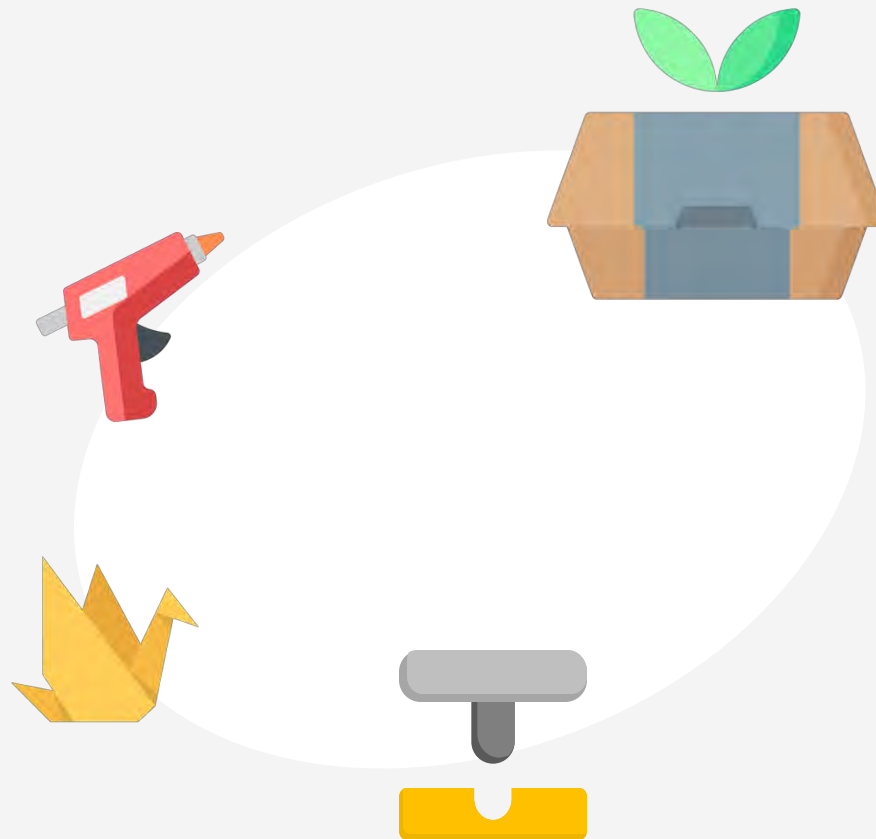
Influenced by **crease rule and matrix geometry, crease stroke**, and material properties

In this study: 2 pt creasing rules.

Induced defects assessed with OGR test at 60 °C

# CONVERTING PROPERTIES AND TRAY FORMING

In collaboration with:



## Tray forming

Press-forming of paperboard trays using heated moulds to impart a shape to a die-cut blank. Parameters that influence the performance are **mould temperature, pressing speed, blank holding force, as well as blank humidity content**

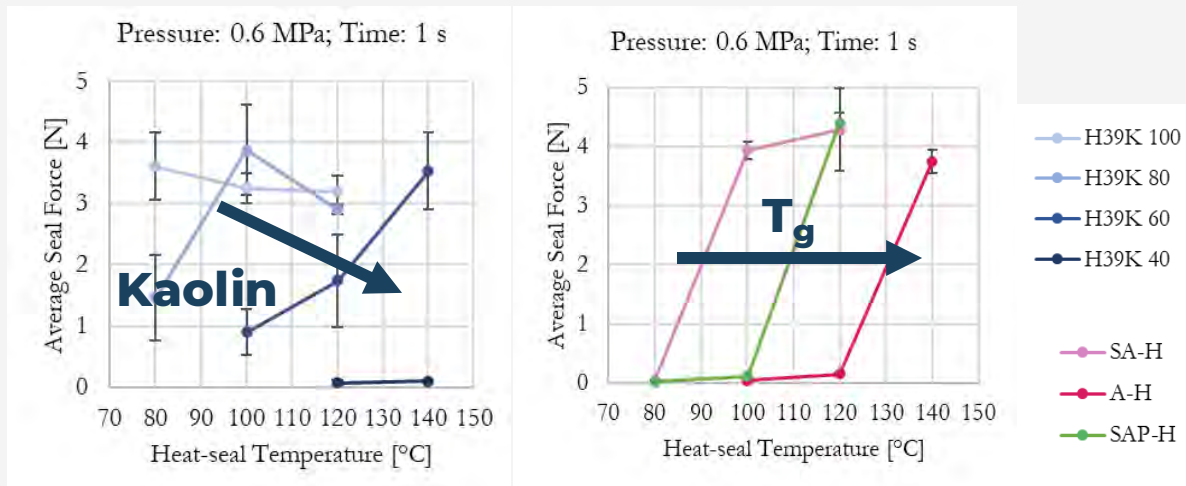
In this study, it was carried out on a pilot machine at industrial processing parameters. Possible coat defects marked with ethanol-based dye solutions

# RESULTS

## Paper – Heat-sealing

**Cohesive failure** occurred at the highest measured forces ( $F \geq 2.5 \text{ N/10 mm}$ ), suggesting the low fibre tear resistance of the substrate

**Kaolin content** is the major factor affecting heat-seal ability. Generally, it is clear how the  $T_g$  plays a crucial role

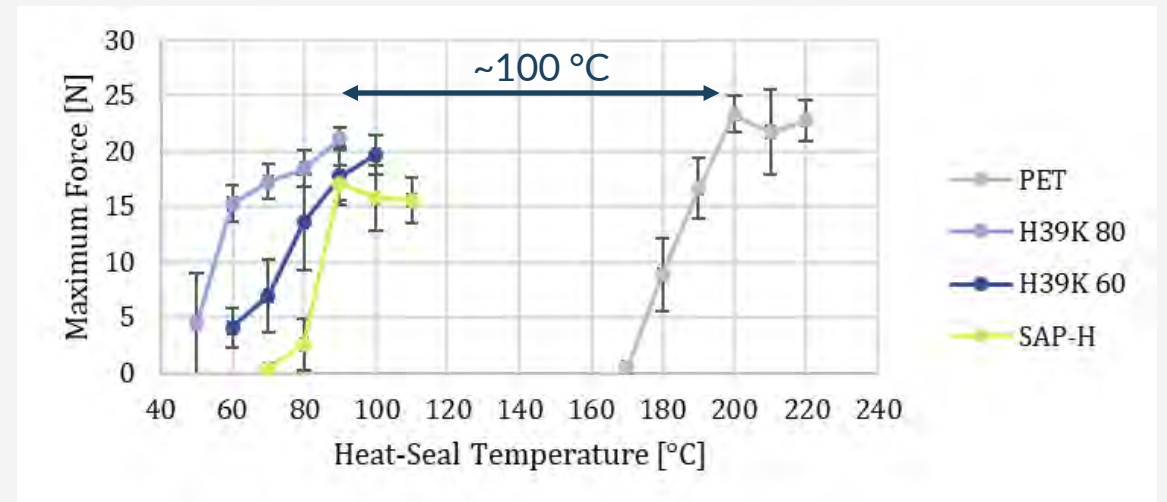


Average seal  $F$  of disp. Coat. ( $t = 1 \text{ s}$ ;  $P = 0.6 \text{ MPa}$ )

## Paperboard – Heat-sealing

The results were similar and coherent to coated paper ones

The graph shows how dispersion coating seal at  **$\sim 100 \text{ }^\circ\text{C}$**  lower compared to PET, possibly beneficial for heat-sensitive content



Max seal  $F$  of disp. Coat. vs extrusion coated PET ( $t = 1.5 \text{ s}$ ;  $P = 2.5 \text{ MPa}$ )

# RESULTS

## Paper – Fold cracking

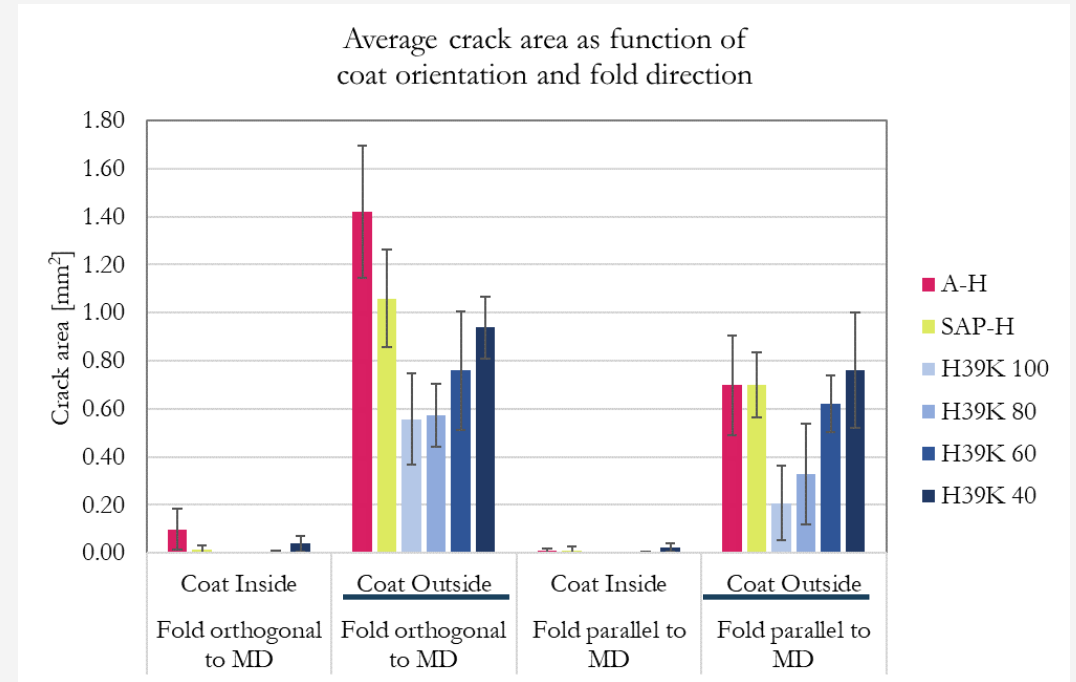
Fold under 10 N for 1 s. Dyed water was applied and overall crack area measured with ImageJ

**Coat outside** is subjected to tensile stresses, showing how they broadly affect coat intactness. Cross Direction ( $CD \perp MD$ ) folding leads to more damage

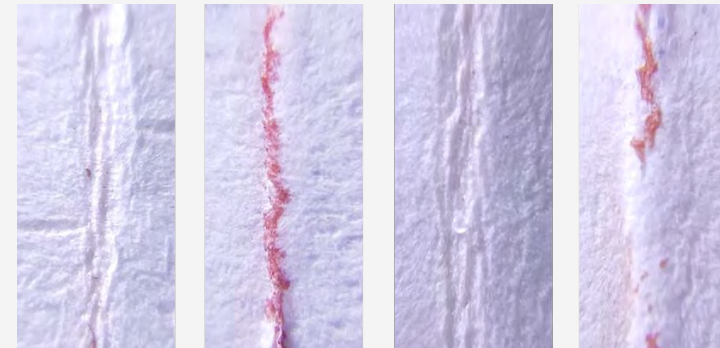
Commercial grades show poorer fold resistance due to lower **latex flexibility** (i.e., higher  $T_g$ )

**Kaolin content** embrittles the coating

Fold cracking influence barrier properties, e.g., **WVTR**, leading to an increase of up to twofold



H39K 60



# RESULTS

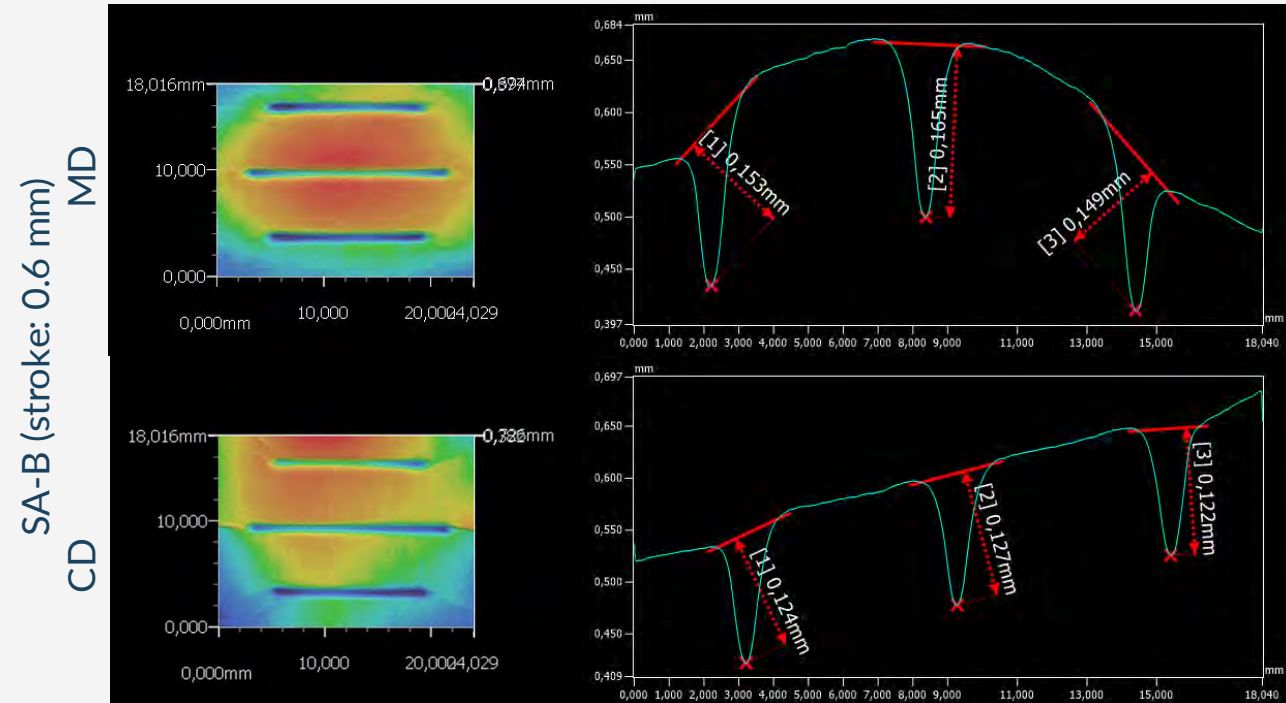
## Paperboard – Creasing

Conventional creasing tool parameters (2 pt., 0.4/1.2 crease matrix)

Crease depth was up to 160  $\mu\text{m}$ . Machine Direction (MD) achieved higher residual depth compared to CD

Coat integrity (modified version of BS ISO 16532-1) provided quite outstanding results for both experimental and SAP-H grades

Due to higher brittleness at  $T_{\text{amb}}$  ( $T_g > T_{\text{amb}}$ ), SA-B showed some crease-induced defects





# RESULTS

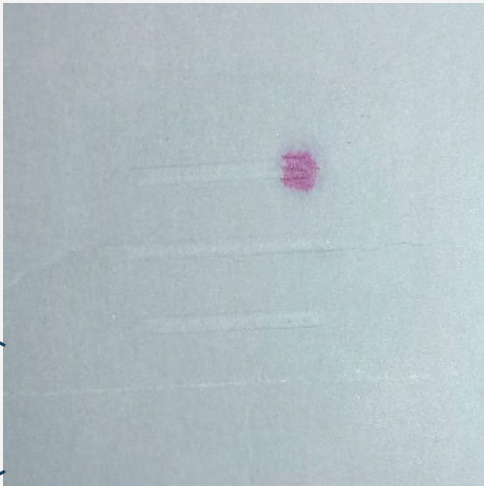
## Paperboard – Creasing

Grease permeation resistance

Stroke [mm]	Direction	H39K 80	H39K 60	SA-B1	SAP-H	SA-B1+SAP-H	PET
0.5	MD	6 < X < 24 h	6 < X < 24 h	180	>24 h	6 < X < 24 h	>24 h
0.5	CD	6 < X < 24 h	6 < X < 24 h	180	>24 h	6 < X < 24 h	>24 h
0.6	MD	6 < X < 24 h	6 < X < 24 h	150 *	>24 h	360 *	>24 h
0.6	CD	6 < X < 24 h	6 < X < 24 h	180 *	>24 h	360 *	>24 h

\* Crease-induced defects were observed.

Crease-induced defect  
(SA-B1)



Crease-induced defect  
(SA-B1) – front side



Grease permeation at  
24 hours (TF PET)



Grease permeation at  
24 hours (H39K 80)

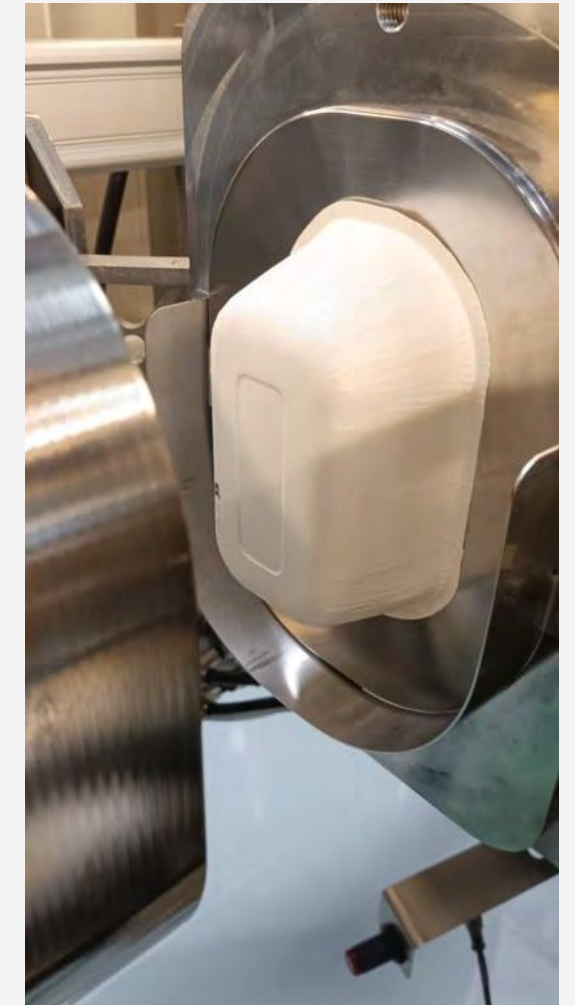
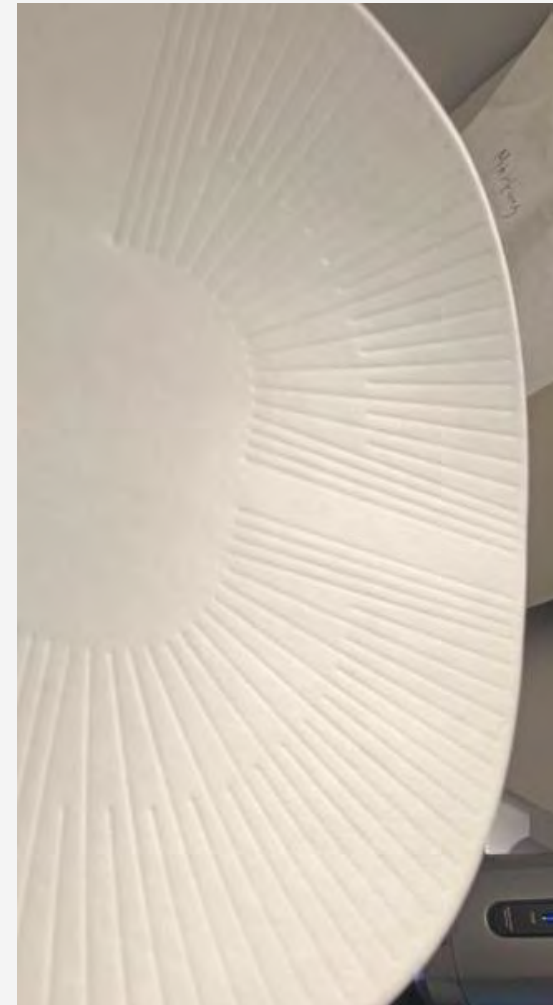
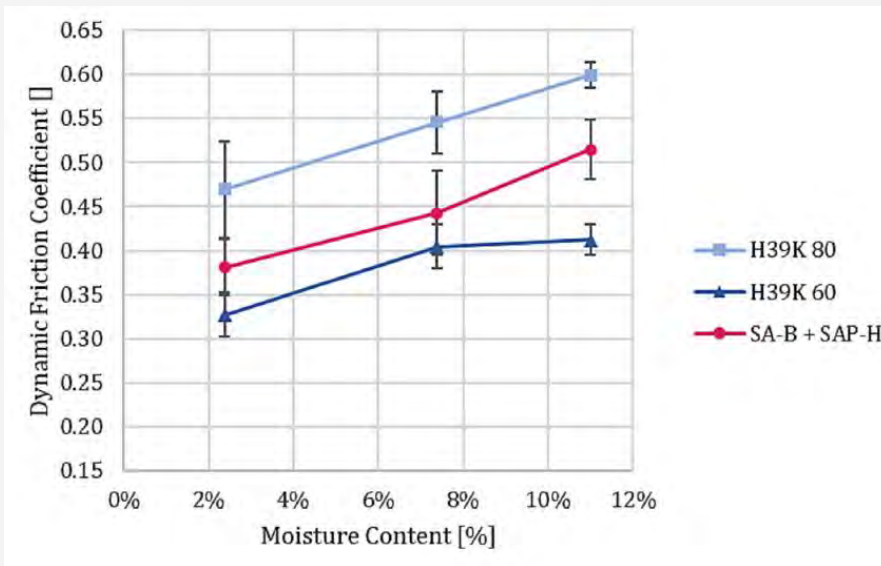


# RESULTS

## Paperboard – Tray forming

Performed on die-cut tray blanks to achieve 1/9 foodstuff container

Humidity content (HC) is crucial not to have blocking. Dispersion coatings required ~4.5% HC, whereas extrusion coating requires ~9% HC



\* The dispersion coating was placed against stainless steel plate.



# RESULTS

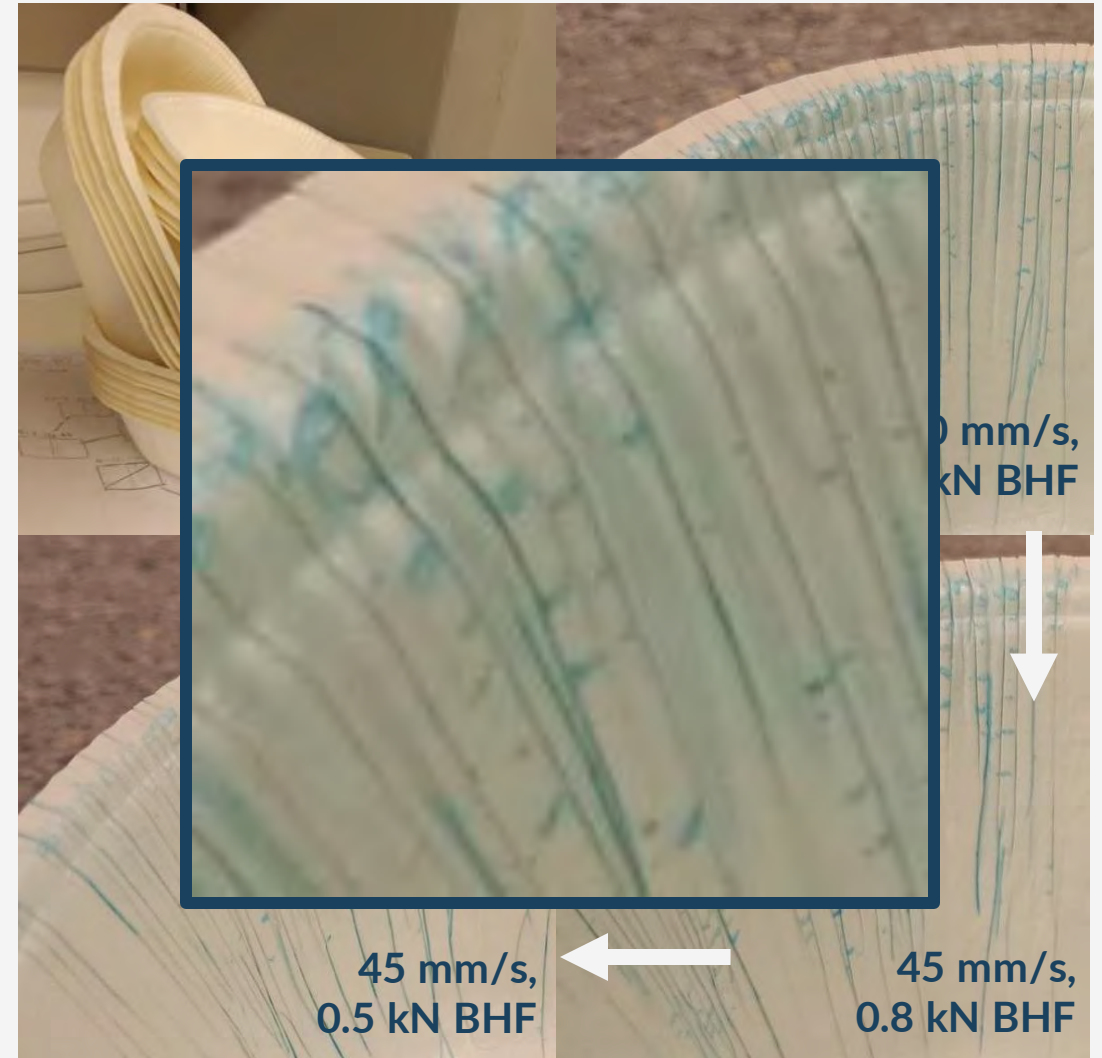
## Paperboard – Tray forming

**Blank Holding Force (BHF)** and **forming speed** are the main parameters to be adjusted. The lower, the better for dispersion coating integrity

This means, however, lower production yields and lower flange smoothness.

**Coat defects** suggested that the thin coatings cannot withstand tensile stresses during the forming process, especially for parameters typically used for extrusion-coated samples

H39K 60  
Humidity Content: 4.5 %  
Mould Temp.: 120 °C





# **RECYCLING AND RECYCLABILITY**

# RECYCLING

## Testing methodologies

### Italy



UNI 11743

### Europe



CEPI version 2

## Evaluation systems

### Italy



Aticelca 501

### Europe



4evergreen alliance

	UNI 11743:2019	Cepi v.2	Notes
Pulping	Yes	Yes	Cepi v.2: samples produced at least 15 (or 30) days before. Possible artificial ageing. pH range for the water.
Filtrate analysis	No	Yes	Evaporation residue is mandatory, COD analysis is optional.
Coarse rejects	Yes	Yes	Cepi v.2: collect all the accept.
Sheet adhesion – intermediate evaluation	No	Yes	
Fine rejects / Flakes	Yes	Yes	UNI: Somerville or Haindl fractionators Cepi v.2: higher fibre quantity, and longer screening time.
Sheet adhesion	Yes	Yes	
Optical inhomogeneity	Yes	Yes	
Macrostickies	Yes	Yes	UNI 11743: slits of 0.10 mm. 10 g batch (can be reduced). Cepi v.2: slits of 0.15 mm. 5 g batch. Optional evaluation.

# RECYCLING



	H39K 80	H39K 60	SA-B1+SAP-H
Coarse reject	2.8 %	0.2 %	0.2 %
Fine reject / Flakes	7.6 %	9.8 %	8.2 %
Macrostickies <2000 µm	58,487 mm <sup>2</sup> /kg	21,271 mm <sup>2</sup> /kg	127,313 mm <sup>2</sup> /kg
Sheet adhesion	Absent	Absent	Absent
Optical inhomogeneity	Level 1	Level 1	Level 1



**Level C**

It could be expected, since they heat-seal quite easily (the kaolin content is crucial)



	H39K 80	H39K 60	SA-B1+SAP-H
Coarse reject	1.3 %	0.3 %	0.2 %
Fine reject / Flakes	4.8 %	5.9 %	3.5 %
Dissolved and colloidal solids <10 µm (evaporation residue)	0.8 %	0.8 %	1.1 %
Macrostickies <2000 µm	113,110 mm <sup>2</sup> /kg	10,060 mm <sup>2</sup> /kg	108,410 mm <sup>2</sup> /kg
Sheet adhesion – intermediate evaluation	Absent	Absent	Partial
Sheet adhesion	Absent	Absent	Absent
Optical inhomogeneity	Level 1	Level 1	Level 1



**90/100**



**87/100**



**93/100**

## CONCLUDING REMARKS

- Dispersion coatings represent an **interesting technology**
- **Processing properties** were good; **tensile stress resistance** is crucial, as visible in fold cracking and tray press forming results. **Latex softness** was positively correlated to coat stress resistance. **Fillers** reduced coating resistance
- **Heat-sealable** grades could heat-seal at temperatures as low as 80 °C, meaning possible energy savings for converters
- **Recyclability** is limited (to date) by macrostickies content for heat-sealable grades





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## Any question?

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